ENGINEER international scientific journal

ISSUE 2, 2025 Vol. 3 **E-ISSN** 3030-3893 **ISSN** 3060-5172 SLIB.UZ ibrary of Uzbekistan



A bridge between science and innovation

TOSHKENT DAVLAT TRANSPORT UNIVERSITETI Tashkent state transport university



ENGINEER

A bridge between science and innovation

E-ISSN: 3030-3893 ISSN: 3060-5172 VOLUME 3, ISSUE 2 JUNE, 2025



engineer.tstu.uz

TASHKENT STATE TRANSPORT UNIVERSITY

ENGINEER INTERNATIONAL SCIENTIFIC JOURNAL VOLUME 3, ISSUE 2 JUNE, 2025

EDITOR-IN-CHIEF SAID S. SHAUMAROV

Professor, Doctor of Sciences in Technics, Tashkent State Transport University Deputy Chief Editor Miraziz M. Talipov

Doctor of Philosophy in Technical Sciences, Tashkent State Transport University

Founder of the international scientific journal "Engineer" – Tashkent State Transport University, 100167, Republic of Uzbekistan, Tashkent, Temiryo'lchilar str., 1, office: 465, e-mail: publication@tstu.uz.

The "Engineer" publishes the most significant results of scientific and applied research carried out in universities of transport profile, as well as other higher educational institutions, research institutes, and centers of the Republic of Uzbekistan and foreign countries.

The journal is published 4 times a year and contains publications in the following main areas:

- Engineering;
- General Engineering;
- Aerospace Engineering;
- Automotive Engineering;
- Civil and Structural Engineering;
- Computational Mechanics;
- Control and Systems Engineering;
- Electrical and Electronic Engineering;
- Industrial and Manufacturing Engineering;
- Mechanical Engineering;
- Mechanics of Materials;
- Safety, Risk, Reliability and Quality;
- Media Technology;
- Building and Construction;
- Architecture.

Tashkent State Transport University had the opportunity to publish the international scientific journal "Engineer" based on the **Certificate No. 1183** of the Information and Mass Communications Agency under the Administration of the President of the Republic of Uzbekistan. **E-ISSN: 3030-3893, ISSN: 3060-5172.** Articles in the journal are published in English language.

Analysis of the operating algorithm of switches in local control mode

S.T. Boltayev¹[®], E.Sh. Jonikulov¹[®], M.Y. Khokimjonov¹[®], E.G. Khujamkulov¹[®]

¹Tashkent state transport university, Tashkent, Uzbekistan

This article provides a theoretical and practical analysis of the issues related to local control of railway Abstract: switches at stations operating under electric interlocking (EI) systems. The main objective of the research is to analyze and improve local control schemes that ensure the safe and reliable execution of shunting operations at railway stations. The study compares existing control methods, particularly those performed through central control panels and maneuvering posts, and highlights their operational contexts. Within the research, the structure and operating principles of local switch control based on the four-wire control scheme commonly used in electric interlocking systems are examined. The article investigates how commands issued by the station operator are executed through electromagnetic relays, providing a detailed analysis of relay sequences and their respective functions based on schematic diagrams. The interconnection of control current sources, switch motors, track conditions, and relays within the local control scheme is clearly explained. As a result of the analysis, it is demonstrated that existing control schemes provide a high level of safety and operational reliability at stations. The technical solutions presented by the author can play a significant role in the modernization of electric interlocking systems. Keywords: Switch, local control, shunting column, electric interlocking, station, route, relay, algorithm

1. Introduction

In the conditions of electric interlocking, shunting operations are carried out in two ways:

1. From the control panel — In this case, shunting operations are performed along routes that are locked in the same manner as train routes. The difference is that a shunting signal can open towards an occupied track or a section at the head of the station without a turnout (i.e., without changing tracks). However, it is closed after the train passes or after the first turnout section beyond it is vacated (i.e., the extinguishing of the signal differs from a regular train signal).

2. From shunting columns, posts, and towers — This method is used in cases where not only routed movements are required, but also when shunting is performed by pushing or along short shunting routes where traversing the entire route is not possible or not advisable [1-3].

At stations where large volumes of shunting operations are carried out, electric interlocking devices allow switching the turnouts in shunting areas to local control — this is done through control panels or shunting columns. The appearance of a shunting column is shown in Figure 1 [4].



Figure 1. View of the maneuvering box

2. Research methodology

There are two types of local control schemes for turnouts, and they are used in the following systems:

• Centralized interlocking systems for intermediate stations with relay-based interlocking and a local power supply.

• Route-relay interlocking with blocking routes.

In this article, we will examine and analyze the operation algorithm of the local control scheme for turnouts in the first system



Figure 2. Single-track station layout

To control the turnout using a four-wire scheme (Figure 3.), four wires are laid from the ДСП post to the relay cabinet: P3 and P4 are used to operate the turnout relay

^a
<u>https://orcid.org/0000-0001-7289-</u>7820

^bhttps://orcid.org/0000-0002-1130-0522

 $(12\Pi C)$, while K1 and K2 are used to create the control circuit. From the relay cabinet to the electric drive, nine wires are laid.

https://orcid.org/0000-0002-5018-6005
https://orcid.org/0009-0004-4556-0746



31June, 2025https://doi.org/10.56143/3030-3893-2025-2-31-35A bridge between science and innovation

Journal Engineer

ISSN: 3030-3893

Volume:3| Issue:2| 2025



Figure 3. Four-wire turnout control circuit

At each thrown position of the switch, a control circuit is formed, and its elements are used to display the switch position on the control panel. In the given diagram, the state of the control circuit elements corresponds to the switch's physical (plunger) position. The switch control relays 12CK1 and 12CK are powered with properly polarized current along the network.

Figure 4 shows the algorithm of how the station dispatcher manages and monitors the switch. In order to operate the switch from the control panel, the following steps are performed:

1 - The "+" or "-" switch button is pressed.

2- It is checked that no route is set in the station's paired throat.

3 - The switch section is checked for availability (it must be unoccupied).

 $4-{\rm It}$ is confirmed that the switch is not under local control.

5 - Based on the button pressed, the polarity of the PS relay is changed.

6 - It is checked that the block contact in the electric drive has not been broken.

7, 14 – A bell rings while the switch is changing position.

8, 15 – The electric motor operates for 7–9 seconds. This will be discussed in detail later.

10, 17 – The switch position indication lights up.

 $18-{\rm If}$ a cut or interruption occurs in the switch circuit, a bell rings.

13 – If the above conditions are not met, the switch cannot be operated.

11, 12 – If false occupancy is detected in the switch section, the station dispatcher presses the CAK button.

2025

June,



Figure 4. Algorithm of switch control and monitoring by the station dispatcher



32

Π48 - (35-36)AΠ - ΠC(H) - K2 - 12CK1

$-12CK - K1 - (33-34) A\Pi - M48$

When the CK relay is activated, the neutral and energized anchor contacts connect, thereby creating the switching circuit of the pilus control relay 12 Π K. The green light on the control panel lights up through the previous contact of the 12 Π K relay. During the switch operation or in the incorrect position (vzrez), the control relays at the A Π contacts are turned off, and the green light on the control panel goes out. The incorrect position buzzer is activated through the rear contacts of the CK relay. This buzzer is turned off by pressing the Π 3K button on the \square C Π . When the Π 3K button is pressed, the control remains until recovery. After the switch position is monitored, the control relays turn on again, and the buzzer sounds. To turn it off, the \square C Π removes the Π 3K button and leaves it in this state [5].

The following measures are implemented to prevent improper operation of the control circuit:

• Two switch control relays, 12CK and 12CK1, are connected in series to the control circuit, so that the Π K or MK relay only operates when the neutral and energized anchor states match in these relays. If only one CK relay is used, and its energized anchor sticks after the switch is operated, the \square C Π would incorrectly control the switch position.

• The energized anchor contact of the $12\Pi C$ relay is connected to the control circuit, which is necessary for automatically checking the alignment of the switching contacts after the switch is operated and for turning off the CK relay when the $12\Pi C$ relay is triggered with a reverse polarity current.

• The supply to the 12CK relay comes from the electric drive's auto coupling, which is implemented when the line wires are connected to prevent incorrect operation.

• The control circuit of the 12CK relay has the ability to break the two-pole contacts through the auto coupling when the switch is operated or during the switch's cut-off.

• The 12CK relay circuit opens when the line wires are disconnected or connected.

To switch the switch to the "minus" position, the $\square C\Pi$ presses the 12MK button. Switch operation is only possible when the switch section is clear (in this case, the 2-12C Π relay is on) and the switch is not linked to the route (in this case, the $\square O31$ relay is on). The $\square O31$ relay is a general recurring connection relay for the routes containing the 12th switch. These routes include:

• reception route (ЧПЗ),

• sending route (HO3),

• maneuver routes (M23 and HM13).

Since the 12th switch (see Figure 1) does not enter the reception route of the 3Π path, nor does it connect to the sending or maneuver routes on the 1Π and 3Π paths, these routes are short-circuited through the front contacts of the HO3, M23, and HM13 relays (6/8 Π K). When these conditions are met, the supply circuit with reverse polarity current is formed through the 12 Π C relay (CK Π III5 type).

$$II = \frac{12IIK}{12} = 12MIK = 4IIO31 = 2-12CII = P4 =$$

$- \underline{M}\underline{J} - \underline{12}\underline{\Pi}\underline{C} - \underline{M}\underline{J} - \underline{P3} - \underline{2-12C\Pi} - \overline{4\Pi31} - \underline{12MK} - -\overline{CB} - \Pi \underline{C\Phi} - M$

He control coil of the 12 Π C relay is connected in series with the CB relay. The CB relay, together with the C Φ and

 $\Pi C\Phi$ relays, forms a group of relays to protect the electric motor from overheating during prolonged operation. Upon activation, the CB relay connects the activation circuit of the C3 relay located in the relay cabinet. After activation, the C3 relay closes the front contact in the working circuit of the electric drive and prepares this circuit for the switching of the converter.

The 12 Π C relay closes the working circuit of the switch through its energized anchor and pulled neutral contacts. This circuit passes through the 43-23 current coil of the 12C Π starting relay, the motor coils, and the 11-12 contacts of the A Π auto coupling.

$\Pi \overline{\mathbf{648}} - \overline{\mathbf{12}\Pi \overline{\mathbf{C}}} - \overline{\mathbf{12}\Pi \overline{\mathbf{C}}} - \overline{\mathbf{2} - (\mathbf{11-12})} \overline{\mathbf{A}\Pi} - \overline{\overline{\mathbf{A}}} - \overline{\overline{\mathbf{6K}}} - 9 - \overline{\overline{\mathbf{12}\Pi \overline{\mathbf{C}}}} - (\mathbf{43-23}) \overline{\overline{\mathbf{12}\Pi \overline{\mathbf{C}}}} - \overline{\mathbf{C3}} - \mathbf{M} \overline{\mathbf{648}}$

While the motor is operating and until the switch transfer is fully completed, the neutral armature of the start switch relay is held in a pulled state due to the low-resistance current coil. The relay power is cut off through the 1-4 coil once the 12MK button is released.

From the moment the 12MK button is pressed and the energized anchor of the $12\Pi C$ relay changes, the switch control relay is deactivated, the switch position monitoring is lost, and the buzzing of the switching process in the apparatus is activated.

Once the switch transfer is fully completed, the working circuit is interrupted through the 11-12AII contacts. Since the 12IIC relay is no longer powered through the current coil, it releases the neutral anchor and initiates a two-pole break of the working battery. After that, a reverse-polarity current closes the control circuit to activate the control relay.

$\Pi 48 - (36-24-23)A\Pi - K1 - 12CK1 - 12CK -$

$- K2 - 12\Pi C(\Pi) - (25-26) A\Pi - M48$

When the 12CK and 12CK1 relays are activated, they close their neutral and polarized contacts, thereby forming the "minus" control circuit for activating the 12MK monitoring relay. Through the front contact of the 12MK relay, the yellow % lamp lights up on the control panel, and the buzzing for switch transfer monitoring is turned off.

From the moment the 12MK (12 Π K) button is pressed, the protective circuit elements of the electric motor are activated. After the CB relay in the start-up circuit is activated, it connects a 3000 μ F capacitor—previously charged through the back contact of the CB relay—to the C Φ relay via its front contact. The C Φ relay is activated by the discharge of this capacitor, pulls in the armature, and energizes both the C3 relay and the Π C Φ repeater relay in the relay cabinet. The C3 relay closes the working circuit, which causes the switch to move to the "minus" position.

Once the 12MK button is released and the CB relay is deactivated, the timing process of the protective circuit begins. This timing is carried out by the C Φ relay. Even though it is disconnected from the 3000 μ F capacitor via the CB relay contact, the C Φ relay remains energized and keeps its armature pulled in for 7–9 seconds due to the discharge of a 1000 μ F capacitor. If the circuit operates normally and there are no obstructions, the switch will be fully transferred within this time. After the switch transfer is completed, the motor circuit is turned off through the 11-12AII contacts.

If the switch transfer is delayed or the electric motor runs too long, after 7–9 seconds the C Φ relay releases its armature and deactivates the C3 relay, which results in disconnection of the motor circuit. Restarting the switch is



https://doi.org/10.56143/3030-3893-2025-2-31-35 A bridge between science and innovation



only possible after this time interval ends and the armature of the $\Pi C \Phi$ relay is released.

If false occupancy is detected in the switch section and the 2-12CII relay contacts are open, the duty operator (DCII) must verify that the section is truly unoccupied and that the rail circuits are intact. After verification, they press the CAK button, which activates the CA emergency switch relay.

The contacts of the activated CA relay shunt the open 2-12C Π contacts, forming a startup circuit for energizing the Π C relay.

The control scheme for paired switches is designed so that both switches are operated using a single pair of start buttons, and their transfer occurs sequentially. In this case, the switch located closer to the relay cabinet is always transferred first, followed by the one located farther away [6-7].



Figure 5. Algorithm for switching the turnout to local control

In Figure 5, the algorithm for switching the turnout to local control is shown. To switch to local control, the following operations and conditions must be met:

To switch turnout No. 12 to local control, the station duty officer (DShP) presses the 12PMK button on the control panel (see Figure 3), which activates the 12VPM maneuver permission relay. This relay, through its front contacts, activates the following:

- MC blinking relay
- ВМЛ lamp (located above the 12PMK button, blinking light)
- The self-holding circuit of the 12VPM relay

In the activation circuit of the 12VPM relay, the absence of other local control actions in this turnout group is verified through the back contacts of:

- 4BM relay
- 12BM relay

• **ЧУРМ** relay

The 12VPM relay also prepares the activation circuit of the 12PM maneuver permission relay. This relay is activated only when the following conditions are met:

- No route is set that would interfere with movement through turnout 12, verified by the front contacts of 4II3 and HO3 relays
- The 2/4 protective turnouts are in a position guarding the local control zone, verified by the front contact of the 2/4ΠK relay

If turnouts 6/8 are in the "+" position, the interference monitored by the HO3 relay is bypassed by shunting the HO3 contact through the 6/8PK contact.

The 12PM relay then activates the following seriesconnected relays:

- 12BM (100 Ohm) located at the post
- 12PM repeater relay (4000 Ohm) located in the relay cabinet

Due to the large resistance difference, only the 12PM relay is activated and pulls in the armature.

In the 12PM relay circuit, the presence of the KJ switch inside the local control panel is verified through the front contact of the 4K relay.

When the 12PM relay pulls in, it lights up the JIM lamp on the local control panel, indicating to the maneuver agent that local control is permitted. The agent unlocks the KJI switch, which deactivates the UK relay. A 770 Ohm resistor is connected in parallel to the 12PM relay via the back contact of the UK relay. This reduces total resistance and increases the current enough to activate the 12BM relay at the post.

Upon activation, 12BM confirms that local control has been accepted by the maneuver agent and triggers the following:

- Deactivates the MΓ blinking relay
- Switches the BMJI lamp from blinking to constant light, notifying the DShP that the key has been removed from the local control panel
- Deactivates the 12VPM relay

Through the front contacts of 12BM and 12PM, the MД maneuver decentralization relay in the relay cabinet is activated. This switches the 12 Π C relay from centralized control to local control. From this point on, the maneuver agent can operate the turnout from the trackside box.

By inserting and turning the key in the lock of the trackside box, the agent closes a polarized circuit (either normal or reverse polarity) to activate the 12Π C relay and switch the turnout to the "+" or "-" position.

To monitor turnout switching in local control, a buzzer is installed in the trackside box, which is activated via the 15-16 and $45-46A\Pi$ contacts. In local control, turnout switching is performed without checking if the turnout section is clear, which reduces false checks and speeds up maneuvering operations. However, it also requires the maneuver agent to exercise special caution with each turnout operation to avoid switching the turnout under a moving train.

After the maneuver is completed, the turnout is returned to central control. The maneuver agent inserts the local control key back into the lock on the local control panel, activating the 4K relay. Through the front contact of the 4K relay, the 770 Ohm resistor is disconnected from the 12BM relay's main circuit. As a result, total resistance increases



34

and the current decreases to a level where the 12BM relay deactivates.

However, if the 2-12CII turnout section has not yet been cleared by the maneuvering train, the 12BM relay remains energized via the local circuit.

3. Conclusion

According to the analysis of the article, reliable and effective operation of local and central control of switches in electric interlocking systems requires complex yet precise relay-based systems built on specific algorithms. The study emphasizes that each component involved in the control, monitoring, and protection mechanisms of switch management must accurately perform its designated function. The local control mode enables maneuvering operations to be carried out quickly and efficiently, while also demanding the reinforcement of safety measures. As a result, the schemes and algorithms presented in the article play a crucial role in ensuring the safety of train movements at modern railway stations.

References

[1] Казаков А.А., Бубнов В.Д., Казаков Е.А. Станционные устройства автоматики и телемеханики. «ТРАНСПОРТ». 431 стр.

[2] Переборова А.С. Телеуправление стрелками и сигналами. «ТРАНСПОРТ». 1981. 390 стр.

[3] Chien, R. T., & Watson, T. J. (1964). Cyclic Decoding Procedures for Bose-Chaudhuri-Hocquenghem Codes. IEEE Transactions on Information Theory, 10(4), 357-363. https://doi.org/10.1109/TIT.1964.1053699.

[4] Карвацкий С.Б., Пенкин Н.Ф., Малинникова Т.В. Телеуправление стрелками и сигналами. «ТРАНСПОРТ». 1985. 224 стр.

[5] Boltaev S.T. Muhiddinov O.O. Joniqulov E.Sh. Ganijonov B.B. Transport xabarnomasi - Journal of Transport - Вестник транспорта. vol. 1 issue 4 2024

[6] Boltayev, S.T., & Kosimova, Q.A. (2022). Railway Point Machine Control Automation Methods. In Proceedings - International Ural Conference on

Measurements, UralCon (Vol. 2022-September, pp. 290-294). Institute of Electrical and Electronics Engineers Inc. https://doi.org/10.1109/UralCon54942.2022.9906687.

[7] Boltayev, S.T., Rakhmonov, B.B., Kasimova, Q.A., & Joniqulov, E.S. (2023). Intelligent Control Systems at Stations for Different Categories of Trains. In AIP Conference Proceedings (Vol. 2612). American Institute of Physics Inc. https://doi.org/10.1063/5.0114539.

Information about the author

Boltayev Sunnatillo Tuymurodovich	Head of the Department of Automation and Telemechanics, Tashkent State Transport University, PhD, Professor. E-mail: <u>sunnat 3112@list.ru</u> Tel. +998909571088 <u>https://orcid.org/0000-0001-7289- 7820</u>
Jonikulov	Doctoral Student at the
Egamberdi	Department of Automation and
Shavkat ugli	Telemechanics, Tashkent State
	Transport University. E-mail:
	egamberdijoniqulov@gmail.com
	Tel.: +998911022797
	https://orcid.org/0000-0002-1130- 0522
Khokimjonov	
Muhammadaziz	Assistant at the Department of Automation and Telemechanics,
Yursunali ugli	Tashkent State Transport
i ui sunan ugn	University. E-mail:
	hokimjonov9494@gmail.com
	Tel.: +998901651994
	https://orcid.org/0000-0002-5018- 6005
Khujamkulov	Assistant at the Department of
Eldorbek	Automation and Telemechanics,
Gayratjon ugli	Tashkent State Transport
Gayracjon ugn	University. E-mail:
	xujamkuloveldor916@gmail.com
	Tel.: +998903317209
	https://orcid.org/0009-0004-4556-
	0746



Inne.

<i>G. Ibragimova, Sh. Kayumov, M. Abduvaitova</i> Analysis of the transport sector and ensuring transport safety in the context of globalization
D. Mukimova Study of the influence of roller disk thickness on the performance indicators of the device9
<i>I. Karimov, I. Abduazimova</i> Determining the elasticity of the contact suspension of electrified railways
J. Narimanov, N. Abdujabarov, D. Aliakbarov, K. Rakhimkariev Maximizing efficiency in solar-powered UAVs: the role of MPPT algorithms in energy harvesting
<i>N. Sulaymonov, D. Hakimov, K. Matrasulov</i> Improving organizational and technological mechanisms for the development of outsourcing services in transport logistics enterprises: Literature Review
<i>A. Yangiboyev</i> <i>The issues of using synthetic fuel in diesel transportation</i> 24
<i>I. Maturazov, D. Sarsenbayev</i> <i>Technology for improving the post-flight maintenance process of</i> <i>aircraft</i>
S. Boltayev, E. Jonikulov, M. Khokimjonov, E. Khujamkulov Analysis of the operating algorithm of switches in local control mode
<i>M. Sultonov, B. Akmuradov</i> <i>The application of energy-saving technologies in parallel computing</i> <i>systems</i>
T. Kurbaniyazov, A. Bazarbayev Analysis of measurement of harmonic power of non-sinusoidal currents in modern electrical networks